

Statistical features of magnetic noise in mixed-type impact fracture

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We study the statistical features of magnetic noise accompanying the dynamic fracture of steel samples during mixed type fracture, where the overall ductile character of crack propagation is interrupted by a sudden brittle jump. The structure of the voltage time series is investigated by identifying discrete peaks which correspond to elementary steps of the jerky cracking process. We show that the height, duration, area, and energy of peaks have power law distributions with exponents falling close to the corresponding values of pure ductile fracture. For single peaks a power law correlation of the height and area with the width is evidenced, however, the mixed nature of fracture gives rise to a crossover between two regimes of different exponents. The average pulse shape of micro-cracking events has a parabolic form with a right handed asymmetry similarly to quasi-static fracture propagation. The asymmetry emerges due to stress localization at the advancing crack front.

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Dynamic fracture of heterogeneous materials plays a significant role in a broad range of industrial applications from machine engineering to the safety of large scale constructions. For the assesment of the dynamic fracture strength of materials a detailed understanding of the initiation and propagation of cracks is essential¹. Contrary to static fracture, the precise experimental characterization of dynamic fracture toughness is still a challenging problem. One of the main issues of experimental techniques is the determination of the onset time of crack propagation which is typically done by crack-tip monitoring using high speed photography, single wire fracture gages, or strain gages^{1,2}. Due to the disorder present at the micro- or meso-scales of construction materials the propagation of cracks has been found to be a jerky process composed of discrete jumps which give rise to the emission of acoustic waves^{3,4}. Dynamic fracture propagation in ferromagnetic materials like steel is also accompanied by magnetic emission (ME) which yields an important alternative to acoustic testing^{2,5}. Such crackling noise measurements can help to overcome the limitations of traditional techniques. Recently, the integrated ME signal has been suggested to be capable to detect fracture initiation, however, the reliability of the method is not satisfactory^{2,5}. More information is encoded in the structure and evolution of the ME time series of crackling events which can complement studies with integrated signals⁶. To work out well-established experimental techniques based on ME analysis with a high reliability a comprehensive understanding of the statistics and dynamic origin of ME signals is needed⁶.

In the present paper we investigate dynamic crack propagation by means of the magnetic emission technique focusing on the case of mixed fracture where the overall ductile character of crack advancement is interrupted by a sudden jump characteristic for brittle fracture. We extend the standard ME analysis of the integrated statistics of pulse quantities by studying the shape of single pulses and the correlations of pulse characteristics. We demonstrate that the mixed-mode fracture gives rise to a

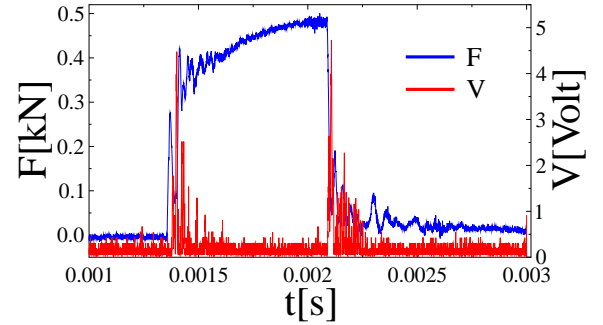


FIG. 1. Force F and voltage V signal of magnetic emission measured during the impact fracture of a V-notched JRQ RPV specimen. The overall ductile propagation of the crack is interrupted by a short brittle period indicated by the sudden force drop accompanied by an intensive generation of high voltage pulses.

crossover in the width-height or width-area correlation of crackling pulses, i.e. power law correlations are pointed out, however, different exponents are obtained for small- and large-sized pulses, typical for ductile and brittle crack propagation, respectively. The average temporal profile of single bursts proved to have a parabolic shape with a right handed asymmetry which is the consequence of stress localization at the propagating crack front.

In order to investigate dynamic fracture of steel, experiments were carried out by means of the Charpy impact machine^{5–7}. The machine itself is a large size pendulum which is raised to a certain height and hits the specimen at the bottom of its swing. The specimens had the dimensions $1\text{cm} \times 1\text{cm} \times 5\text{cm}$ according to the standards of Charpy tests⁷. Steel specimens were carefully manufactured in order to minimize the initial mechanical stress and damage inside the material. The velocity of the hammer of the impact machine had the same value $v_0 = 5.5\text{m/s}$ in all the experiments. In order to control

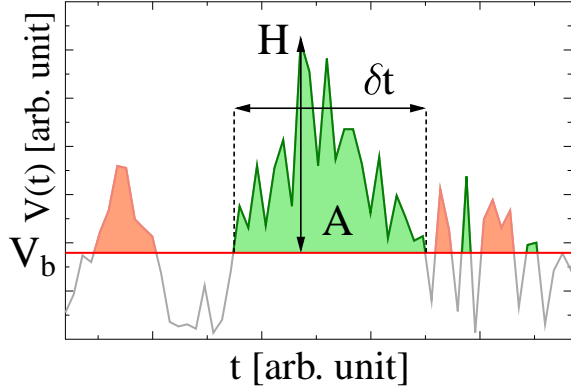


FIG. 2. Identification of peaks and the definition of peak quantities such as height H , duration δt , and area A .

the position of the crack initiated by the energetic hit the specimens were either pre-cracked or V-notched in the middle. Samples were made of two different types of steel, i.e. reactor pressure vessel steel *JRQ RPV* was used for both pre-cracked and V-notched specimens, while carbon steel *S355J2* was only used for V-notched samples. Since the material of the samples has ferromagnetic properties the propagation of the crack is accompanied by changes of the magnetic field. The ME activity was recorded in the form of a voltage signal by a small-sized coil attached to the impactor. Recently, it has been shown that this magnetic noise provides interesting insight into the dynamics of crack propagation being sensitive to fluctuations of the speed of the crack front and of the opening of the crack^{5,6}. Parallel to magnetic noise we also measured the force acting on the moving impactor. The sampling rate was $\Delta t = 5 \times 10^{-7}$ s which provided sufficient resolution at our impact velocity v_0 .

Figure 1 presents an example of the voltage signal $V(t)$ and of the force $F(t)$ measured simultaneously during an impact fracture experiment. Note that the type of fracture, i.e. either brittle or ductile can be inferred from the $F(t)$ curve: brittle fracture implies the sudden initiation of a crack running through the sample which gives rise to a sudden drop-down of the force after a short uploading. The gradual evolution of $F(t)$ observed in the figure is characteristic for ductile fracture where stable crack propagation emerges. In our experiments all specimens had mixed-fracture, i.e. the crack propagation started in a ductile manner, however, the sudden fall of the force indicates a brittle jump of the crack which was then again followed by stable propagation (see Fig. 1). In spite of the complex cracking process, the force curve varies relatively smoothly, the wavy pattern is caused by elastic waves traveling through the sample. However, the voltage signal shows strong fluctuations with a complicated structure along the entire fracture process. Note that the brittle regime of fracture typically gives rise to a more intense magnetic activity with higher and broader peaks⁶.

In order to characterize the structure of magnetic noise accompanying dynamic fracture we decompose the voltage time series into a sequence of discrete peaks following the method presented in Ref.⁶. Note that the method is analogous to the evaluation technique of Barkhausen noise measurements^{8–11}. As a first step we identify the background noise level V_b by searching for the most probable voltage value. Then peaks are identified as segments of the $V(t)$ time series between two intersections with the background V_b . In a single sample a few hundred voltage peaks are identified where peak i starts at time t_i^s and ends at t_i^e . In order to characterize single peaks a set of quantities are determined by carefully evaluating the measured voltage signals, see Fig. 2 for illustration: The overall geometry of peaks is characterized by their height H_i and width, i.e. the peak duration δt_i . The height H_i of peak i is the largest voltage value $V_i^{max} = \max[V(t)(t_i^s \leq t \leq t_i^e)]$ in the peak duration from which the background is subtracted $H_i = V_i^{max} - V_b$. The peak duration δt_i is obtained as the difference of the ending t_i^e and starting times t_i^s as $\delta t_i = t_i^e - t_i^s$. The area A_i of peak i is calculated as the integral of the voltage curve above the background level (see Fig. 2), while for the energy of the peak E_i the square of the voltage signal is integrated in a similar way

$$A_i = \int_{t_i^s}^{t_i^e} (V(t) - V_b) dt, \quad E_i = \int_{t_i^s}^{t_i^e} (V(t) - V_b)^2 dt. \quad (1)$$

It has been shown in Ref.⁶ that peaks of magnetic noise can be associated to elementary events of dynamic crack propagation. Due to the stochastic nature of crack propagation all quantities defined above have strong fluctuations, hence, for the characterization of the voltage time series we determined the probability distributions and the correlations of peak quantities. In order to improve the statistics of the data experiments were repeated 5, 7, and 12 times for pre-cracked, V-notched JRQ RPV, and for V-notched carbon steel, respectively.

The primary quantities characterizing the shape of peaks are the width δt and height H . Figure 3(a) presents the probability density of peak heights $p(H)$ for all three sets of experiments. Power law decay of $p(H)$ can be observed for large values of H

$$p(H) \propto H^{-\beta}, \quad (2)$$

where the exponent β has nearly the same value $\beta = 1.55 \pm 0.15$ for all types of samples. The corresponding distribution of peak durations $p(\delta t)$ has also a power law asymptotics

$$p(\delta t) \propto \delta t^{-\alpha} \quad (3)$$

persisting over three decades in δt (see Fig. 3(b)). The value of the exponent can be determined with a relatively good precision $\alpha = 1.67 \pm 0.06$. Note that due to the low statistics of the data in the large δt regime it is hard to infer the shape of the cutoffs limiting the power

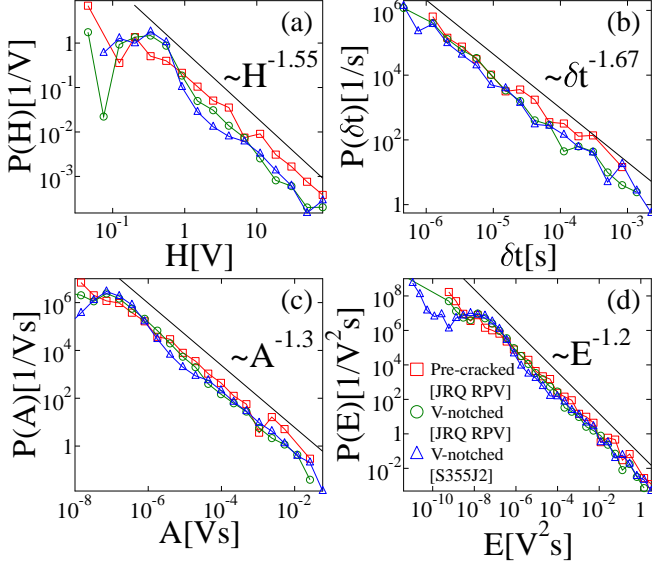


FIG. 3. Probability distributions of the height H (a), duration δt (b), area A (c), and energy E (d) of voltage peaks. Power law functional form is evidenced in all cases.

laws. The area A and energy E defined by Eqs. (1) provide measures for the magnitude of crackling events represented by the peaks. The probability distributions of peak area $p(A)$ and energy $p(E)$ are presented in Figs. 3(c, d), where a power law functional form is evidenced for both distributions over several orders of magnitude

$$p(A) \propto A^{-\tau}, \quad p(E) \propto E^{-\epsilon}. \quad (4)$$

The exponents were obtained numerically as $\tau = 1.3 \pm 0.05$ and $\epsilon = 1.2 \pm 0.05$. The power law character of single peak quantities implies that the jerky steps of crack propagation are not random but correlations occur between consecutive jumps of the crack front. Ductile cracks advance in small steps as the hammer of the impact machine proceeds. In case of brittle fracture the crack decouples from the impactor and it leads to sudden failure with a small number of large jumps⁶. Consequently, brittle and ductile cracking are characterized by lower and higher exponents of the distributions of peak quantities⁶. A very interesting outcome of our measurements is that mixed type fracture is also characterized by power law distributions which are naturally dominated by the peaks generated in the ductile regime.

Of course, single peak quantities are not independent of each other, i.e. it can be expected that a broader peak has a larger height and in turn a larger magnitude represented by the peak area and energy. Such correlations of the peak height H and duration δt can be quantified by the conditional average, i.e. averaging H for fixed values of δt . Figure 4(a) shows that the average height $\langle H \rangle$ has a power law dependence on the width of peaks δt

$$\langle H \rangle \propto \delta t^\xi, \quad (5)$$

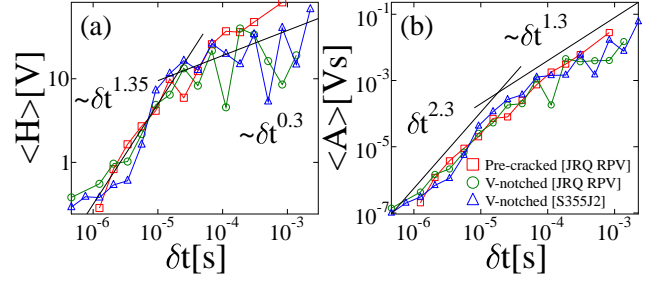


FIG. 4. Correlation of peak quantities. Average height $\langle H \rangle$ (a) and average area $\langle A \rangle$ (b) of peaks as a function of the peak duration δt . Power law dependence is obtained with a crossover between two regimes of different exponents.

however, the value of the exponent ξ has a distinct change at a characteristic peak duration δt_c . The crossover between the two power law regimes of different exponents occurs at $\delta t_c \approx 2 \times 10^{-5}$ s and the exponent ξ takes the values $\xi = 1.35$ and $\xi = 0.35$ below and above δt_c , respectively. The statistics of the data in Fig. 4(a) is somewhat lower above the crossover point $\delta t > \delta t_c$ which is consistent with the rapid decrease of $p(\delta t)$ in Fig. 3(b). The result implies that for broad peaks $\delta t > \delta t_c$ the height increases slower with the width than for the narrow ones. Note that the crossover is not visible on the probability distributions $p(H)$ and $p(\delta t)$. A possible explanation is that both the height and duration values above the crossover fall in the cutoff regime of the distributions.

Based on Eq. (5) we can assume the approximate relation $H \propto \delta t^\xi$ from which a scaling relation of the exponents α and β of $p(\delta t)$ and $p(H)$ can be derived as

$$\alpha = 1 + \xi(\beta - 1). \quad (6)$$

Substituting the value of the exponents the scaling form is fulfilled with a good precision below the crossover duration but not above δt_c since the exponents α and β are dominated by the ductile regime of crack propagation. Based on the height-width relation of pulses the area A can be simply approximated as a function of δt

$$A \propto \delta t^{1+\xi}. \quad (7)$$

To test the validity of the above form we determined the conditional average $\langle A \rangle(\delta t)$ by directly averaging A in bins of δt . Figure 4(b) demonstrates that power law behavior is obtained as expected with the same crossover behavior that has been found for the peak height (see Fig. 4(a)). The values of the exponent 2.3 and 1.3 below and above the crossover point are consistent with Eq. (7).

The correlation of the height, area, and duration provides a characterization of the overall shape of single crackling peaks. A more detailed description can be obtained by determining the average temporal profile $\langle V(t, \delta t) \rangle$ of pulses of a fixed duration δt ^{11,12}. Since single voltage pulses correspond to individual steps of the

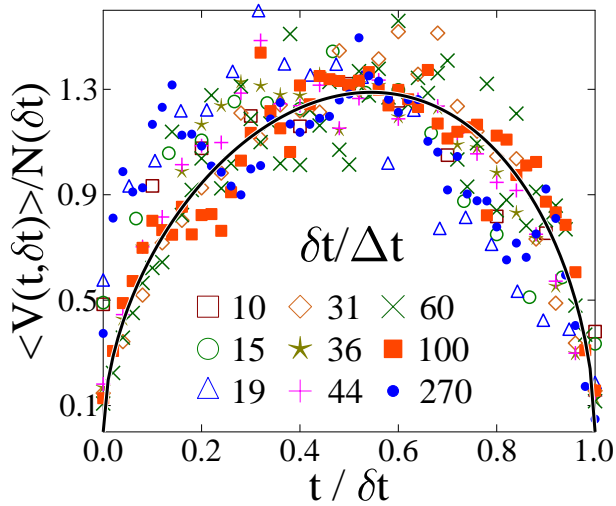


FIG. 5. Average temporal profile of pulses rescaled with $N(\delta t)$ varying the duration $\delta t/\Delta t$ in a broad range from 10 to 270. The continuous line represents best fit with Eq. (9).

advancing crack, the average temporal profile provides information about the time evolution of intermittent crackling bursts. To improve the statistics, pulses of duration $\delta t \pm 0.1\delta t$ were averaged together using the data of all measurements. Figure 5 presents that rescaling $\langle V(t, \delta t) \rangle$ with the norm $N(\delta t) = \int_0^1 \langle V(t/\delta t) \rangle d(t/\delta t)$, pulse profiles of different duration δt can be collapsed on a master curve as a function of the normalized time $t/\delta t$. It follows from Eq. (7) that the norm scales as $N(\delta t) \sim \delta t^\xi$ so that the good quality data collapse implies the validity of the scaling form of pulse shapes

$$\langle V(t, \delta t) \rangle = \delta t^\xi f(t/\delta t). \quad (8)$$

The scaling function $f(x)$ has a parabolic shape which shows that during crackling jumps the crack front starts slowly then it accelerates followed by a gradual slow down^{13,14}. Note that the profile $f(x)$ is slightly skewed to the right indicating the time irreversible nature of the temporal burst dynamics. The same temporal profile has been found very recently for crackling bursts generated at a slowly propagating crack front in heterogeneous materials^{14,15}. It has been shown that the symmetry of the pulse shape carries information about the range of stress redistribution following local breaking events: long range interaction (mean field) results in symmetric profiles, while short range load sharing gives rise to a right handed asymmetry^{14,15}. It follows that the right handed asymmetry of the pulse shapes in Fig. 5 is the fingerprint of the localized stress redistribution along the crack front during dynamic fracture propagation. The scaling function $f(t/\delta t)$ was fitted with the functional form

$$f(x) \sim [x(1-x)]^\gamma [1 - a(x - 1/2)], \quad (9)$$

where the exponent γ determines the shape of $f(x)$ in the vicinity of $x = 0$ and $x = 1$, while a controls the degree of

asymmetry¹⁵. Best fit was obtained with $\gamma = 0.55$ which is significantly lower than the corresponding mean field value $\gamma = 1$ ^{10,12,14,16}, however, it falls closer to the result on quasi-static planar crack propagation $\gamma \approx 0.78$ ¹⁵. The asymmetry is quantified by the parameter value $a = -0.2$ which has a larger absolute value than the ones predicted by models of static crack propagation^{14,15}.

We studied dynamic fracture of steel by analysing the structure of magnetic emission time series generated by the jerky propagation and opening of a crack. Our analysis revealed that for all types of specimen the height, duration, area, and energy of crackling pulses are all power law distributed with exponents falling close to their counterparts of pure ductile fracture. The mixed (ductile-brittle) nature of the fracture process gives rise to a crossover in the correlation of peak quantities with a sharp transition between two regimes of different exponents. The most remarkable result is that the average temporal profile of crackling peaks has a parabolic form with a right handed asymmetry similarly to pulse shapes characterizing quasi-static crack propagation in heterogeneous materials. Profiles of different durations can be collapsed on a universal master curve on both sides of the crossover point. The asymmetry of pulse shapes can be attributed to stress localization at the propagating front. The results imply that the time evolution of ME peaks is the same at the onset of crack propagation as later in the regime of stable propagation since it is solely determined by the range of stress redistribution. To obtain information on the onset time of fracture the analysis has to go beyond single peak quantities and involve e.g. the waiting time between consecutive crackling events.

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